



Template-free synthesis of cubic-rhombohedral-In₂O₃ flower for ppb level acetone detection

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ABSTRACT

Analyzing volatile organic compounds in exhaled breath is a noninvasive method that has potential for disease assessment. Herein, acetone sensors based on porous In₂O₃ flowers are synthesized through a facile solvothermal method. Structural characterizations demonstrate that the three-dimensional In₂O₃ flower-like structure comprises porous ultrathin two-dimensional nanosheets. The structural porosity results in a large specific surface area and fast gas diffusion, which can improve the gas sensing performance. The crystalline structure of the prepared hierarchical flower-like In₂O₃ is a mixed phase of rhombohedral and cubic phases according to the XRD patterns. The sensing properties of the cubic-rhombohedral In₂O₃ (bcc-rh-In₂O₃) are also investigated. Compared with commercial-In₂O₃-based sensor, the bcc-rh-In₂O₃ sensor exhibits 2.9 times higher response ($R_a/R_g = 12$) and shorter response time (ca. 2 s) toward 50 ppm acetone. The bcc-rh-In₂O₃ sensor has a low detection limit of 10 ppb in atmosphere and can easily distinguish acetone from ethanol. The extraordinary properties of the bcc-rh-In₂O₃ sensor are mainly attributed to the n-n heterojunction between rh-In₂O₃ and bcc-In₂O₃.

1. Introduction

Health inspections have gained increasing attention given the continuous improvement of the quality of human life [1–3]. Among available inspection methods, breath analysis is nonintrusive, easy to operate, and fast in obtaining results [4,5]. Gas chromatography can reveal about 3000 volatile organic compounds in human breath; about 200 gases among them are associated with diseases, such as lung cancer, breast cancer, diabetes, and liver disease [6]. Studies have reported that acetone concentration in exhaled air is related to ketone content in blood. The concentration of acetone in breath of healthy individuals should be less than 0.9 ppm, and levels above 1.8 ppm may suggest insulin-dependent diabetic ketosis [7]. A number of scholars have focused on acetone detection. In particular, sensors based on semiconducting metal oxides are of great interest because of their low cost, adjustable performance, and simple device structure [8–10].

The concentrations of most target gases are very low [11]; as such, superior sensing characteristics are required for precise detection. In 2003, Yamazoe et al. [12] reported three key factors in sensor design, namely, receptor function played by the surface of each oxide grain, transducer function played by each grain boundary, and utility factor

related to the sensing body. Various strategies have been proposed as follows in accordance with the principles. The first strategy is design of various morphologies, such as nanocubes [13], nanoparticles [14], nanospheres [15], nanoflowers [16], nanotubes [17], nanofibers [18], nanorods [19], inverse opal structures [20], and urchin-like structures [21]. The second strategy is construction of heterostructures. Zhang et al. [22] fabricated In₂O₃/CuO sensors, which exhibited 5 times higher response to ethanol than CuO sensors. The third strategy is doping or loading catalysts. Ma et al. [23] synthesized 0.5 wt% Pt-loaded WO₃ sensor, which shows 5.6 times higher response to CO than the unloaded material.

In₂O₃ is a typical n-type semiconducting metal oxide with a wide band gap and a promising candidate for solar cells [24], touch displays [25], photocatalysts [26], and gas sensors [27] due to its brilliant electrical and optical features. In₂O₃ is a polymorph, i.e., a cubic bixbyite-type In₂O₃ (bcc-In₂O₃, $E_g: 2.93 \pm 0.15$ eV) and a rhombohedral corundum-type In₂O₃ (rh-In₂O₃, $E_g: 3.02 \pm 0.15$ eV) [28–30]. The formation of InOOH is a key step for obtaining rh-In₂O₃, and the presence of In(OH)₃ promotes the formation of bcc-In₂O₃ [31,32]. Single-phase In₂O₃ has been fabricated by annealing corresponding precursors. For example, Liu et al. [33] synthesized In₂O₃ octadecahedron

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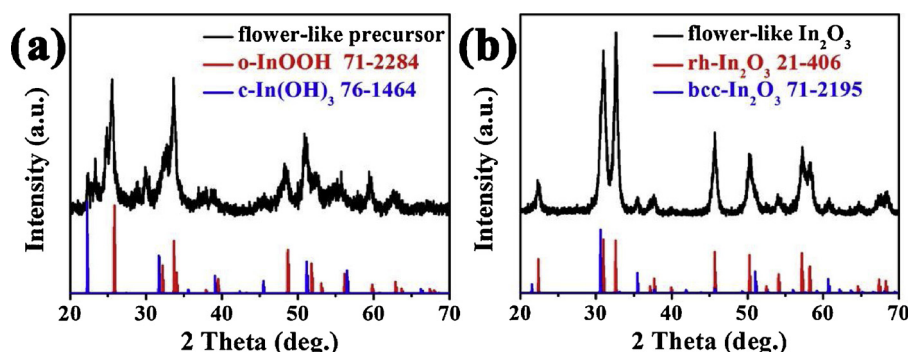


Fig. 1. XRD patterns of the sample: (a) before calcination, (b) after calcination at 400 °C.

by annealing an 18-facet $\text{In}(\text{OH})_3$ precursor. Wang et al. [34] synthesized In_2O_3 cubes after annealing $\text{In}(\text{OH})_3$ at 500 °C. Singhal et al. [35] prepared $\text{rh-In}_2\text{O}_3$ with a rice-grain type morphology by thermal dehydration of InOOH nanostructures. However, compared with $\text{bcc-In}_2\text{O}_3$, $\text{rh-In}_2\text{O}_3$ has been rarely studied due to its harsh synthesis conditions, such as high temperature and high pressure [36,37]. In previous research, $\text{rh-In}_2\text{O}_3$ is mainly used in photoelectric devices [38] and photocatalysts [39]; few reports are available on its use in gas sensors [40]. Moreover, few works have investigated acetone sensors based on mixed-phase flower-like In_2O_3 .

In this study, we successfully fabricated hierarchical porous flower-like cubic-rhombohedral In_2O_3 ($\text{bcc-rh-In}_2\text{O}_3$) nanostructures through a facial one-step solvothermal route followed by calcination. The sensors based on the as-obtained materials exhibited superior gas sensing properties toward acetone in terms of high response, short response time, low detection limit, and good selectivity. The sensing mechanism was discussed according to the morphology and crystal phase of the sensing materials.

2. Experimental

2.1. Material synthesis

The commercial indium oxide (In_2O_3 , 99.995%) was purchased from Nanjing Cinor Chemical Technology Co., Ltd.. Indium nitrate hydrate ($\text{In}(\text{NO}_3)_3 \cdot 4.5\text{H}_2\text{O}$, 99.5%) and glycerol ($\text{C}_3\text{H}_8\text{O}_3$, 99%) were obtained from Sinopharm Chemical Reagent Co., Ltd.. Ethanol ($\text{C}_2\text{H}_6\text{O}$, 99.7%) was purchased from Beijing Chemical Works. All of the chemicals were of analytical reagent grade. Deionized water was used throughout the experiment. The synthesis process of $\text{bcc-rh-In}_2\text{O}_3$ is presented as follows.

In brief, $\text{bcc-rh-In}_2\text{O}_3$ was prepared by a simple solvothermal route. Firstly, 15 mL of deionized water was mixed with an equal volume of ethanol and stirred on a magnetic stirring plate. Subsequently, 0.3 g of $\text{In}(\text{NO}_3)_3 \cdot 4.5\text{H}_2\text{O}$ (0.786 mmol) and 8 mL of glycerol were dissolved in the mixture. A Teflon-lined stainless steel autoclave was used as a reaction vessel to hold the reactants. The reaction temperature and time were set as 180 °C and 1 h, respectively. The as-synthesized sediment was collected by centrifugation and purified using deionized water and ethanol solution. The dried sediment was annealed at 400 °C for 2 h to obtain $\text{bcc-rh-In}_2\text{O}_3$.

2.2. Material characterization

The crystal structure identification was performed by X-ray diffraction (XRD), using a Rigaku D/Max 2550 X-ray diffractometer with $\text{Cu K}\alpha$ radiation ($\lambda = 1.5418 \text{ \AA}$) in the 2θ range of 20–70°. Surface morphologies and microstructures were characterized by scanning electron microscope (SEM, JEOL JSM-7500 F). The transmission electron microscopy (TEM), high-resolution TEM (HRTEM) images were

obtained by a JEOL JSM-2100 F transmission electron microscopy. The N_2 adsorption-desorption isotherms were measured by a Micrometrics Gemini VII 2390 analyzer. The surface area data and pore size distribution were obtained by the Brunauer-Emmett-Teller (BET) model and Barrett-Joyner-Halenda (BJH) methods, respectively.

2.3. Fabrication and measurement of gas sensors

The manufacturing and test processes of the sensor were the same as reported previously [41]. An alumina tube was coated with $\text{bcc-rh-In}_2\text{O}_3$ slurry. Subsequently, a Ni-Cr alloy coil was inserted into the tube. The tube and the coil were soldered on a plastic base to form a sensor, which was aged in air at 250 °C for more than 2 days. Commercial In_2O_3 powder (99.995%) was purchased from Nanjing Cinor Chemical Technology Co., Ltd. and used to fabricate hand-made sensors for comparison with sensors based on $\text{bcc-rh-In}_2\text{O}_3$. The sensor based on commercial In_2O_3 was also fabricated in exactly the same way. Gas sensing performance was evaluated by static testing method. The temperature and humidity of air in atmosphere were approximately 30 °C and 40%RH, respectively. Low concentrations of acetone were obtained from 100 ppm acetone gas, and the other concentrations were obtained from acetone liquid. Response was defined as R_a/R_g (reducing gases) and R_g/R_a (oxidizing gases), where R_a and R_g are the resistance of the sensor in air and target gas, respectively. Response and recovery time were defined as the time taken to achieve 90% of the total resistance change.

3. Results and discussion

3.1. Structural and morphological characteristics

The XRD pattern of the sample before calcination is shown in Fig. 1a. Most peaks can be indexed to the orthorhombic phase InOOH (o-InOOH , JCPDS NO. 71-2284) or the cubic phase $\text{In}(\text{OH})_3$ ($\text{c-In}(\text{OH})_3$, JCPDS NO. 76-1464). Fig. 1b demonstrates the XRD pattern of the as-obtained product after calcination. All of the diffraction peaks can be indexed to the rhombohedral phase In_2O_3 ($\text{rh-In}_2\text{O}_3$, JCPDS NO. 21-406) or the cubic phase In_2O_3 ($\text{bcc-In}_2\text{O}_3$, JCPDS NO. 71-2195). Hence, the In_2O_3 product is a mixed phase material. Furthermore, the formation mechanism of the mixed phase was investigated.

As early as 2004, Yu et al. [31] reported that the final phase of the In_2O_3 product is greatly affected by the precursor. When the precursor is o-InOOH , the final product is rhombohedral In_2O_3 . The $\text{c-In}(\text{OH})_3$ precursor is the key to the formation of cubic In_2O_3 . Therefore, we infer that the $\text{bcc-rh-In}_2\text{O}_3$ mixed phase in the present work was derived from the mixed phase of the precursor. At the reaction temperature (180 °C), the solvents including ethanol (boiling point: 78.3 °C) and deionized water (boiling point: 100 °C) were mostly in the gas state and glycerol (boiling point: 290 °C) was almost in the liquid state. The liquid glycerol acted as the main reactant and combined with In^{3+} to form o-InOOH

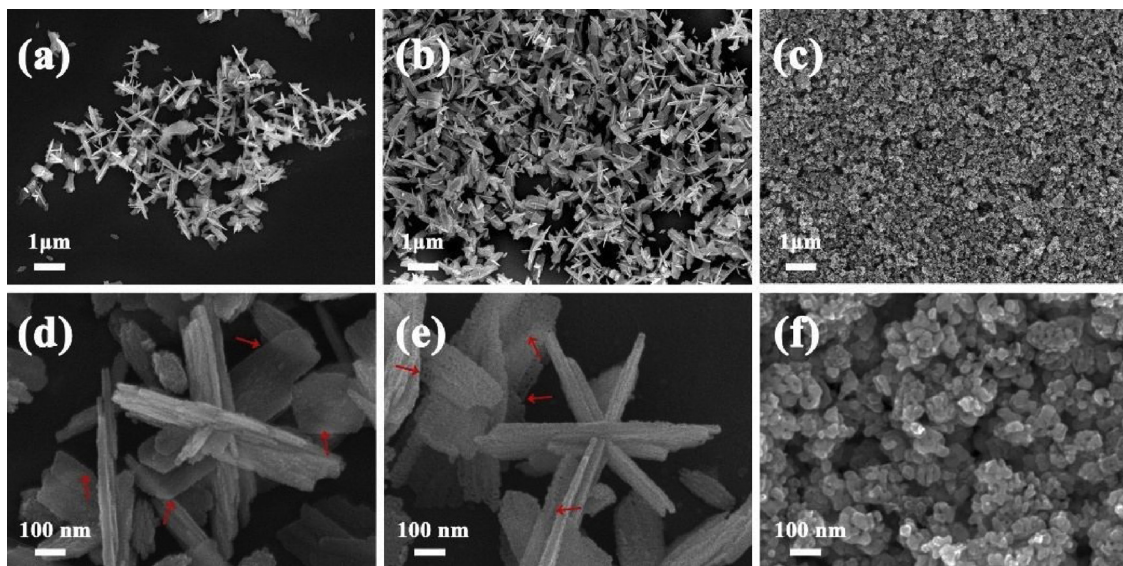


Fig. 2. SEM images of the sample: (a) and (d) before calcination, (b) and (e) after calcination at 400 °C, and (c) and (f) the commercial In_2O_3 .

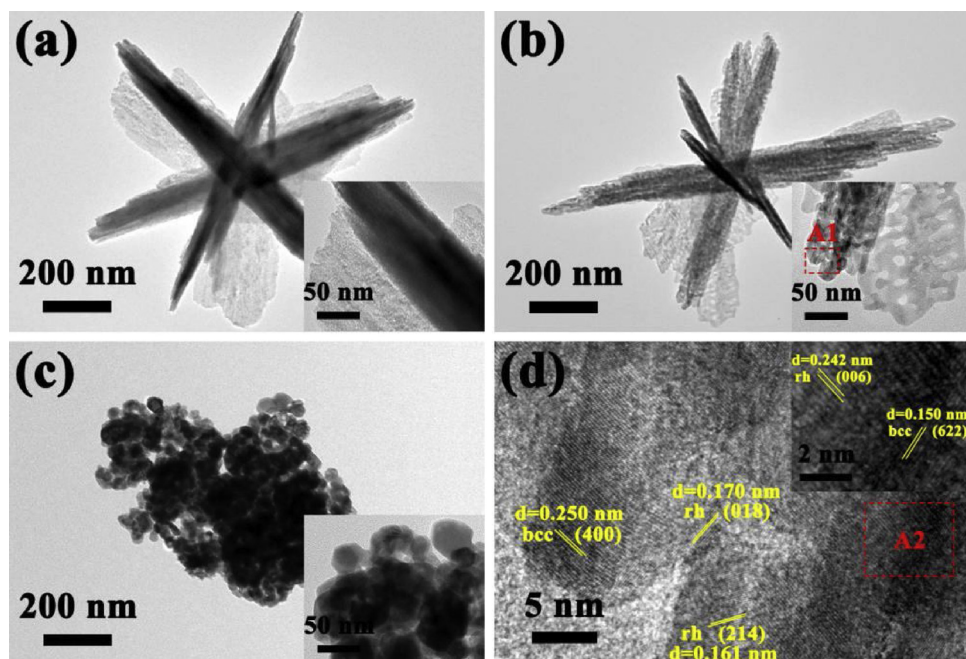


Fig. 3. TEM image of the sample (a) before annealing and (b) after annealing, (c) TEM image of the commercial In_2O_3 ; the insets in Fig. 3a–c are the high-magnification images; (d) HRTEM image of area A1 in the sample after annealing; the illustration is an enlarged image of area A3.

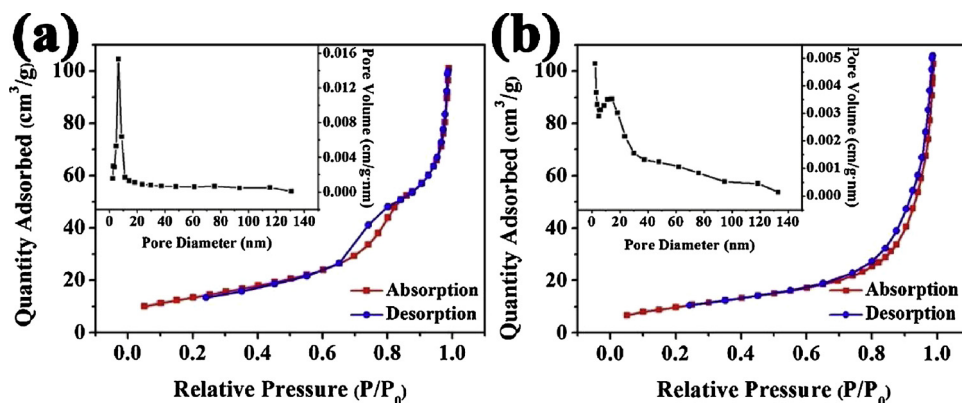


Fig. 4. N_2 adsorption-desorption isotherms of (a) the bcc-rh- In_2O_3 and (b) the commercial In_2O_3 ; the illustration is the pore size distribution plots.

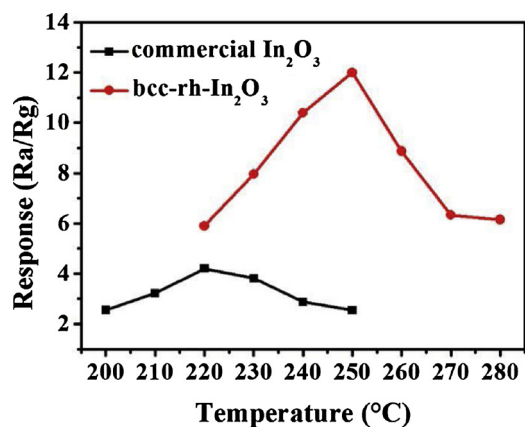
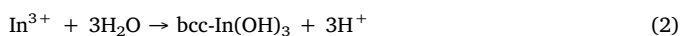
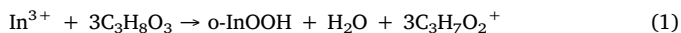


Fig. 5. Responses of sensors based on commercial In_2O_3 and bcc-rh- In_2O_3 to 50 ppm acetone as a function of the operating temperature.

precursor. Given the small amount of liquid water, bcc- $\text{In}(\text{OH})_3$ was synthesized.



Glycerol would form hydrogen bonds with InOOH , contributing to the stabilization and formation of InOOH [42]. A precursor containing o- InOOH and bcc- $\text{In}(\text{OH})_3$ was prepared, and the product containing rh- In_2O_3 and bcc- In_2O_3 was obtained after annealing.



The surface morphology of the sample before calcination is presented in Figs. 2a and d. The precursor possesses a flower-like hierarchical microstructure with a diameter of approximately 1 μm and assembly of several coarse sheets with a high length-to-thickness ratio. As pointed by the arrows in Fig. 2d, some of the sheets are so thin that

the other sheets behind them can be seen directly. After calcination, the In_2O_3 product maintained a flower-like morphology with almost the same size as the precursor (Fig. 2b). The nanosheets of the flower are more porous and rougher than the precursor, as indicated by the arrows in Fig. 2e. As shown in Fig. 2c and f, commercial In_2O_3 has irregular grain-like morphology and more agglomerated configurations. Therefore, the sensing film formed by the accumulation of the bcc-rh- In_2O_3 microflowers possesses more gaps and allows the target gas to diffuse into the sensing body more easily than the commercial In_2O_3 sensing film. The porous flower-like hierarchical microstructure might offer abundant frameworks for gas diffusion and benefit gas sensing properties [43].

TEM images reveal that the In_2O_3 flower consists of several nanosheets before and after annealing. The diameter of the flower is about 1 μm , which fits the value estimated from the SEM images. As presented in Fig. 3a and b, the nanosheets become more porous and rougher after calcination. The pores are highly interconnected, providing a channel for the transfer of gas molecules and improving the gas sensing properties. Comparison between the flower-like In_2O_3 and the commercial In_2O_3 indicates that the latter could not disperse well and might be difficult to be fully accessible for the target gas. Fig. 3d shows two crystal phases in the flower. Inter-planar distances of 0.250 and 0.150 nm present a good fit to the (400) and (622) planes of bcc- In_2O_3 , respectively. The lattice spacings of 0.161, 0.170, and 0.242 nm are consistent with the (214), (018), and (006) planes of rh- In_2O_3 , respectively. The results confirm the existence of a mixed phase, consistent with the XRD pattern.

N_2 adsorption-desorption profiles (Fig. 4) were characterized to clarify the porousness of the samples. Based on the IUPAC classification, the adsorption-desorption isotherms of bcc-rh- In_2O_3 and commercial In_2O_3 can be classified as type IV isotherms. The pore size distribution curve (inset of Fig. 4a and b) was calculated from the desorption branch. The hierarchical In_2O_3 flower displays a narrow pore size distribution centering at approximately 7 nm, implying the formation of a mesoporous structure (2–50 nm) in the sample. The commercial In_2O_3 exhibits a relatively wide pore size distribution centering at approximately 14 nm. In addition, the BET surface areas of the bcc-rh- In_2O_3

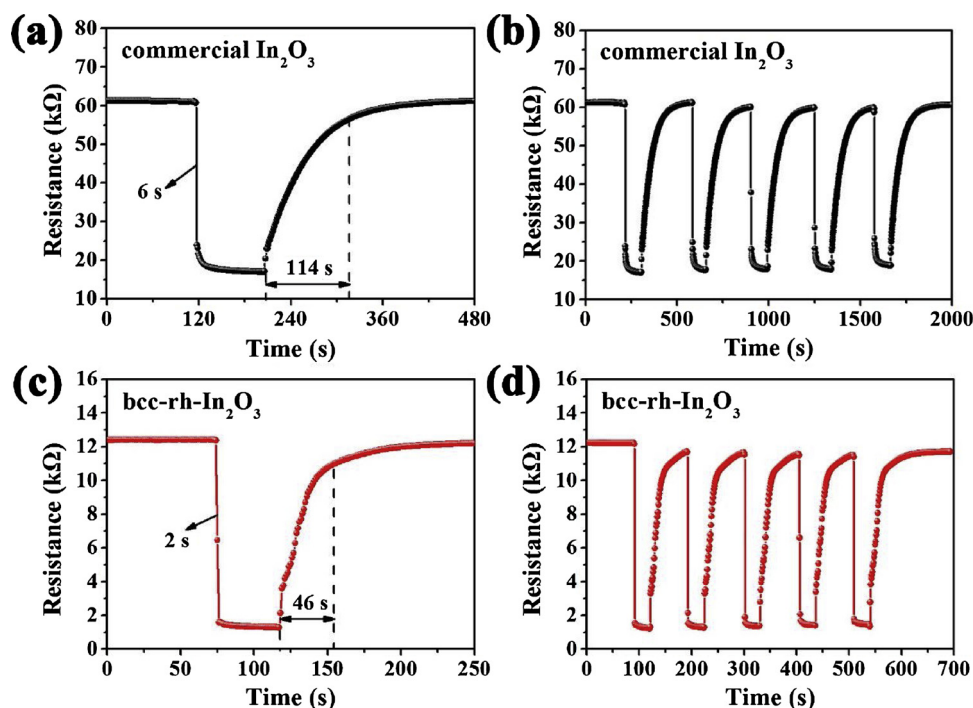


Fig. 6. Dynamic response-recovery curves of the sensor based on (a) commercial In_2O_3 and (b) bcc-rh- In_2O_3 exposed to 50 ppm acetone at their own optimum working temperatures; five reversible cycles of the sensor based on (c) commercial In_2O_3 and (d) bcc-rh- In_2O_3 .

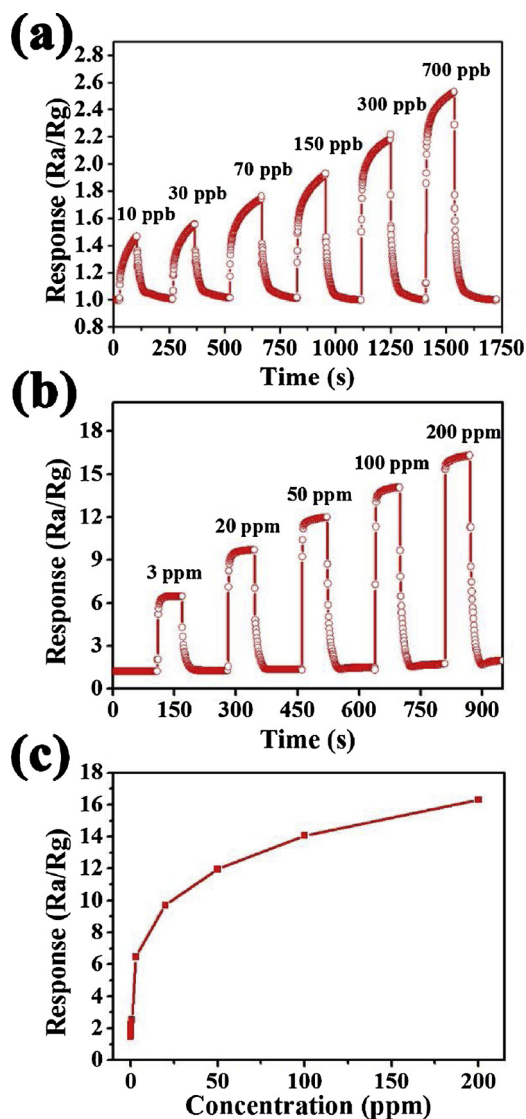


Fig. 7. Time-dependent response curves of the bcc-rh-In₂O₃ sensor to acetone within a range of (a) 10–700 ppb and (b) 3–200 ppm at 250 °C; (c) responses of the bcc-rh-In₂O₃ sensor to 10 ppb–200 ppm acetone at 250 °C.

and the commercial In₂O₃ are 48.6 and 36.7 m²/g, respectively. The large surface area might contribute to more surface active sites and enhance the sensing properties of the sensors based on bcc-rh-In₂O₃ [44].

3.2. Gas-sensing properties

The surface states of the sensing material are strongly affected by

Table 1
Comparison of acetone sensing ability of diverse In₂O₃ gas sensors^a.

Material	Temp. (°C)	Conc. (ppm)	Res. (Ra/Rg)	Tres/Trec (s)	Detetion Limit (ppb)	Ref.
In ₂ O ₃ microflowers	250	50	13.6	2/46	10	Our work
Inverse opal In ₂ O ₃ microspheres	275	100	13.2	1/51	83.3	[1]
In ₂ O ₃ nanofibers	300	100	6.6	2/32	500	[46]
In ₂ O ₃ hollow microspheres	350	50	11.11	–	500	[47]
In ₂ O ₃ blocks	370	50	9.35	–	–	[48]
Sb-doped In ₂ O ₃ films	200	80	4	–	–	[49]
Au-doped In ₂ O ₃ nanofibers	300	100	12.4	2/9	–	[50]
flower-like In ₂ O ₃ microspheres	250	200	9.72	5/182	–	[51]

^a Temp, temperature; Conc, concentration; Res, response (Ra/Rg); Tres/Trec, response time/recovery time; Detetion Limit, low detection limit; Ref, reference.

the operating temperature; thus, exploring the optimized working temperature is necessary [45]. In this test and the following experiments, the hand-made sensor fabricated by the commercial In₂O₃ powder was compared with the sensor based on bcc-rh-In₂O₃. As presented in Fig. 5, the responses of these two sensors first increased and then decreased with increasing working temperature. The maximum response of the sensor based on bcc-rh-In₂O₃ reached 12.0 at 250 °C, whereas the sensor based on commercial In₂O₃ achieved the largest response of 4.2 at 220 °C. The optimized working temperatures for further experiments are 250 °C and 220 °C for the sensor based on bcc-rh-In₂O₃ and commercial In₂O₃, respectively.

Fig. 6a and c shows the dynamic response-recovery curves of the sensor based on commercial In₂O₃ and bcc-rh-In₂O₃ to 50 ppm acetone, respectively. The resistance of the sensors, especially the bcc-rh-In₂O₃ sensor dropped quickly as soon as they were exposed to the acetone vapor. Once placed in the air ambient, the resistance recovered to their initial states. The response and recovery time are 2 and 46 s for the bcc-rh-In₂O₃ sensor, and 6 and 114 s for the sensor based on commercial In₂O₃. The test was performed for five cycles, as shown in Fig. 6b and d. The results confirm that both sensors show good stability and reversibility after alternate exposure to air and acetone vapor.

The responses of the bcc-rh-In₂O₃ sensor to low concentrations of acetone (< 1 ppm) and high concentration of acetone (≥ 3 ppm) were tested and plotted in Fig. 7a and b, respectively. The corresponding response increased with increasing acetone concentration, exhibiting typical concentration-dependent response curves. The responses to 10, 30, 70, 150, 300, and 700 ppb acetone are 1.5, 1.6, 1.8, 1.9, 2.2, and 2.5, respectively. The responses to 3, 20, 50, 100, and 200 ppm acetone are 6.5, 9.7, 12.0, 14.1, and 16.3, respectively. Moreover, Fig. 7c shows concentration dependence of bcc-rh-In₂O₃ sensor response. With increasing acetone concentration, the response of the gas sensor increased. When the concentration of acetone is as high as 200 ppm, the bcc-rh-In₂O₃ sensor do not tend to be saturate even though the increasing trend gradually slows down with increasing acetone concentration. Hence, the bcc-rh-In₂O₃ sensor not only has a relatively low detection limit but also a broad detection range. The gas sensing properties of other sensors based on In₂O₃ nanomaterials are listed in Table 1. Compared with the sensors based on In₂O₃ nanomaterials, the fabricated bcc-rh-In₂O₃ sensor displayed the highest response and acceptable recovery time to acetone.

As demonstrated in the radar graph (Fig. 8a), the response plot of the sensor based on commercial In₂O₃ is surrounded by the response plot of the bcc-rh-In₂O₃ sensor, indicating the higher response of the latter for all target gases. In addition, the angle to acetone is sharpest in Fig. 8a, implying high selectivity of the sensor based on bcc-rh-In₂O₃. The responses of the bcc-rh-In₂O₃ sensor to 50 ppm acetone, ethanol, methanol, xylene, formaldehyde, benzene, toluene, carbon monoxide, and ammonia are 12.0, 2.9, 4.8, 3.1, 4.1, 1.4, and 1.2, respectively. In particular, the bcc-rh-In₂O₃ sensor can more clearly distinguish acetone from ethanol compared with the sensors based on SnO₂ nanomaterials [52–55]. The histogram of responses in Fig. 8b verifies that the optimum working temperatures for detection of ethanol and acetone are

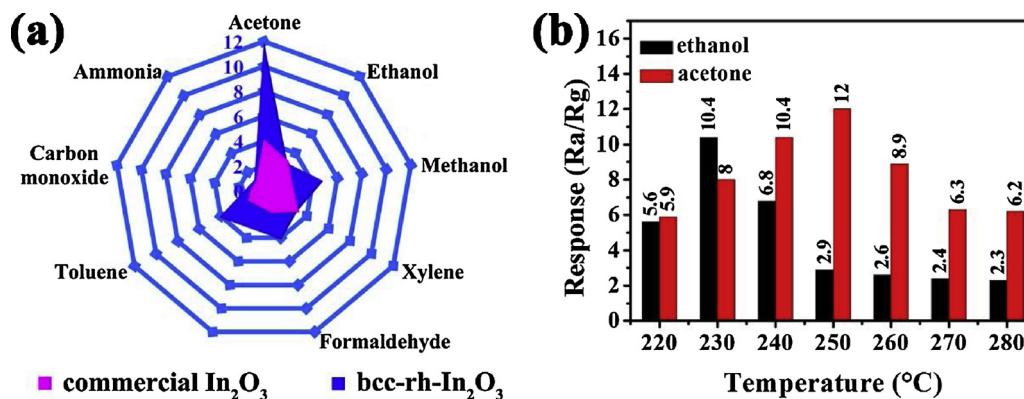
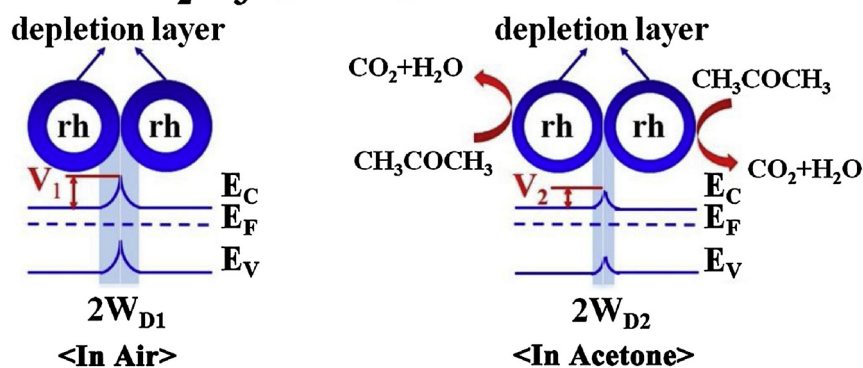


Fig. 8. (a) Responses of the bcc-rh-In₂O₃ sensor and the sensor based on commercial In₂O₃ to 50 ppm various gases at their own optimum working temperatures; (b) Responses of the bcc-rh-In₂O₃ sensor to 50 ppm ethanol and acetone at different working temperatures.

(a) rh-In₂O₃ pure phase



(b) bcc-rh-In₂O₃ mixed phase

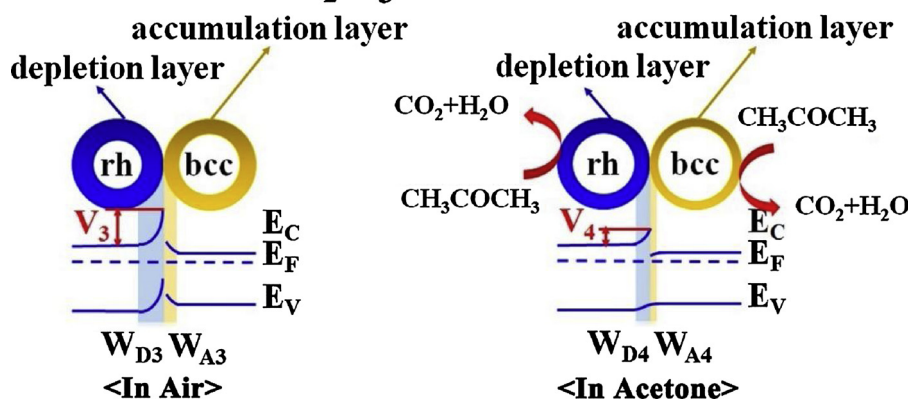


Fig. 9. Energy band diagrams of (a) the rh-In₂O₃ pure phase and (b) the bcc-rh-In₂O₃ mixed phase.

230 °C and 250 °C, respectively. The response to acetone (12.0) is higher than the response to ethanol (10.4) even at their own optimum operating temperatures. At the optimum operating temperature of acetone (250 °C), the response to ethanol decreased from 10.4 to 2.9.

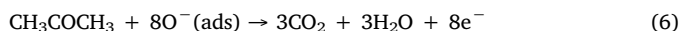
3.3. Gas sensing mechanism

The surface control models and the energy band diagrams of pure rhombohedral phase In₂O₃ are shown in Fig. 9a to provide further insights into the sensing mechanism of the mixed phase In₂O₃. In air, oxygen molecules will be adsorbed on the surface of rh-In₂O₃ and be ionized by capturing electrons from rh-In₂O₃, forming negatively

charged oxygen. The adsorption of negatively charged oxygen will result in the formation of an electron depletion layer (W_{D1}) on the surface of rhombohedral In₂O₃ nanoparticles and increase the potential energy barrier (V_1). The specific reactions are as follows:



Once the sensor is exposed to acetone, electrons trapped in the negatively charged oxygen will be released back to In₂O₃ nanoparticles. Thus, the electron depletion layer became narrow ($W_{D2} < W_{D1}$), and the potential energy barrier decreased ($V_2 < V_1$), leading to increased resistance. The chemical reaction equation is as follows:



Furthermore, the energy band diagrams of the mixed phase In_2O_3 are described in Fig. 9b. The work functions of rhombohedral In_2O_3 and cubic In_2O_3 are 4.3 [56] and 5 eV [57,58], respectively. The Fermi level of rh- In_2O_3 is different from that of bcc- In_2O_3 . Thus, a typical n-n heterojunction would form when the cubic In_2O_3 nanoparticles come in contact with the rhombohedral In_2O_3 nanoparticles. Moreover, electrons would transfer from rhombohedral In_2O_3 to cubic In_2O_3 until the Fermi levels become consistent because the Fermi level of rh- In_2O_3 is higher than that of bcc- In_2O_3 . Therefore, the electron concentration of rh- In_2O_3 is lower than that of pure rhombohedral phase In_2O_3 . A wider electron depletion layer ($W_{D3} > W_{D1}$) and a higher potential energy barrier ($V_3 > V_1$) will form on the surface of rh- In_2O_3 . Furthermore, the accumulation layer between the rh- In_2O_3 and bcc- In_2O_3 nanoparticles helps the adsorption of oxygen and facilitates the reaction of acetone with the sensing body [22]. Therefore, the gas sensor based on bcc-rh- In_2O_3 nanomaterials can achieve high gas response to the target gases. Besides, flower-like structures can accelerate gas diffusion into the sensor body and enhance the utility factor of the gas sensor. The porous structure of the nanosheets also facilitates the enhancement of the gas sensing characteristics because of the contribution to the high BET area and target gas fluxion in the microflower. Such structure properties also ensure the fast response and recovery speed of the gas sensor [59].

4. Conclusion

In summary, the acetone sensors based on bcc-rh- In_2O_3 flower-like hierarchical structure demonstrate better gas sensing performance compared with those based on commercial In_2O_3 . The high response, low detection limit, short response/recovery time, and outstanding selectivity are mainly attributed to the extraordinary N-n heterojunction. The porous and hierarchical structure also contributes to the high response and fast response/recovery speed. Results reveal that the mixed phase In_2O_3 is a good candidate for the fabrication of acetone gas sensors.

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